

Towards the Integration of Graphoepitaxial High- T_c SQUIDs into Multichannel MEG Systems

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We have assessed the possibility to construct multichannel magnetoencephalography (MEG) systems based on high- T_c direct current superconducting quantum interference devices (DC SQUIDs) with graphoepitaxial step-edge Josephson junctions [1]. A new layout of multilayer high- T_c superconducting flux transformers was tested and a new type of high- T_c DC SQUID magnetometer intended for MEG systems was realized. These magnetometers have vacuum-tight capsules of outer diameter 24 mm and a magnetic field resolution of ~ 4 fT/ $\sqrt{\text{Hz}}$ at 77 K. Crosstalk between adjacent sensors was estimated and measured for in-plane and axial configurations. The vibration-free cooling of sensors, minimization of the sensor-to-object distance, optimization of the sensor positions and gantry design are discussed. Our findings have implications for the next generation of non-invasive imaging techniques that may be used to understand human brain function.

The importance of developing a new generation of non-invasive imaging techniques that can be used to understand human brain function is reflected, for example, in the "Human Brain Project" (EU) and the "BRAIN Initiative" (USA). Multichannel MEG systems that are based on low temperature SQUIDs are well developed and used routinely for the non-invasive investigation of multiple time-dependent sources of weak magnetic field generated by the human brain. MEG systems that are based on sensitive high- T_c SQUIDs promise to improve signal-to-noise ratio and to provide better source characterization by reducing the SQUID-to-scalp separation [2]. A single-channel MEG system based on high- T_c DC SQUID flip-chip magnetometers with a 16 mm x 16 mm multilayer flux transformer has achieved a magnetic field resolution of ~ 4 fT/ $\sqrt{\text{Hz}}$ at 77.4 K [3], which is similar to the magnetic field resolution of individual channels in commercial MEG systems based on 28 mm x 28 mm low- T_c SQUIDs (Elekta Neuromag). The first source localization of brain

activity using a single channel high- T_c system for MEG was demonstrated recently [4].

We have prepared high- T_c DC SQUIDs by high oxygen pressure magnetron sputtering and deep-UV photolithography of YBCO-SrTiO₃ heterostructures. Oxygen transport through epitaxial SrTiO₃ insulating films is important for resistive switching devices and for oxygenation of the bottom superconducting layer in multilayer high- T_c superconducting flux transformers. The current development of high- T_c SQUIDs is partially supported by the rapid development of metal-oxide heterostructures for applications such as room temperature resistive switching devices. We have observed large bipolar resistive switching in heterostructures that contain YBCO-SrTiO₃ interfaces [5]. A resistance switching ratio over 10^3 and a stable operational endurance over 5000 cycles were observed at room temperature.

The low capacitance of high- T_c Josephson junctions is advantageous for lowering the intrinsic flux noise of high- T_c DC SQUIDs:

$$S_\Phi \approx 32k_B T L (LC / \beta_C)^{1/2}, \quad (1)$$

where $\beta_C = 2\pi I_c R_n^2 / \Phi_0 \approx 0.4$ is the McCumber parameter and $\Phi_0 = 2.07 \cdot 10^{-15}$ T·m² is the magnetic flux quantum. The lower operating temperatures of low- T_c SQUIDs are almost compensated by the typically much higher capacitance of their Josephson junctions (~ 1 pF). This property can explain the comparably high sensitivities of high- T_c and low- T_c SQUIDs, in spite of the much higher operating temperature of high- T_c SQUIDs.

In MEG systems, near-optimal sensitivity of SQUIDs to magnetic fields of ~ 4 fT/ $\sqrt{\text{Hz}}$ at 77.4 K can be provided by a superconducting flux transformer with a 14-turn input coil and a pick-up loop with an outer diameter of 20 mm. Figure 1 shows a photograph of such a flux transformer and a vacuum-tight encapsulated high- T_c magnetometer intended for assembly into a multichannel

MEG system. It encloses a flip-chip high- T_c DC SQUID magnetometer, a feedback coil and a heater.

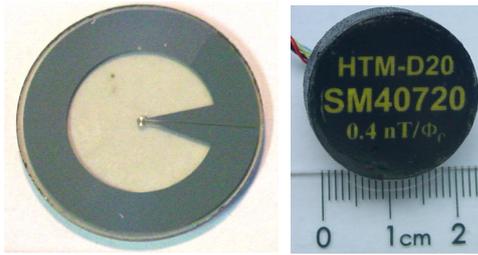


FIG. 1: A multilayer high- T_c superconducting flux transformer with a 20 mm pick-up loop and a 14-turn input coil (left photograph) and an encapsulated DC SQUID containing such a flux transformer (right photograph).

In multi-channel SQUID systems, an important requirement is the prevention of crosstalk between channels. Linearization of the output signal of each SQUID in a multichannel system is provided by feedback signal to each SQUID from its feedback coil. Parasitic inductive coupling between the feedback coil and the pick-up loop of neighbouring sensors should be minimized. Such coupling can be expressed in terms of crosstalk between the SQUID sensors using the ratio between the flux induced by the feedback coil in a test sensor Φ_1 by a nearby inducing sensor and the flux read by the inducing sensor Φ_2 :

$$\frac{\Phi_1}{\Phi_2} \approx \frac{\mu_0 m}{4\pi\Phi_2} \int_{y_0-R}^{y_0+R} \int_{-\sqrt{R^2-(y-y_0)^2}}^{\sqrt{R^2-(y-y_0)^2}} \frac{2x_0^2 - y^2 - z^2}{(x_0^2 + y^2 + z^2)^{5/2}} dz dy, \quad (2)$$

where $R = 1$ cm is the radius of the pick-up loop of the neighbouring magnetometer. The flux Φ_2 induced by the feedback coil in the pick-up loop of the inducing SQUID is:

$$\Phi_2 \approx \frac{\mu_0 m r^2}{2(r^2 + x_0^2)^{3/2}}. \quad (3)$$

The results of the calculation of Eqs. (2) and (3) are shown in Figure 2, while experimentally measured data for Φ_1/Φ_2 are shown in Figure 3.

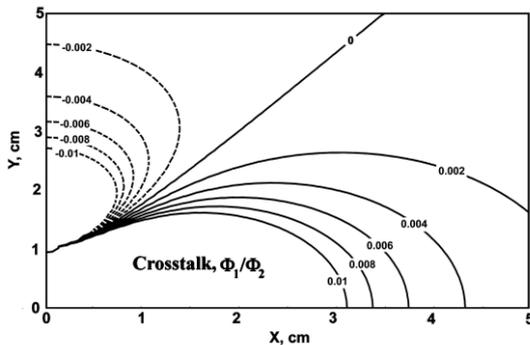


FIG. 2: Crosstalk calculation according to Eqs. (2) and (3).

A crosstalk of below 1 % was achieved at distances of more than 30 mm in both orientations. This measurement confirms the possibility to build close-packed arrays of high- T_c SQUID magneto-

meters with the proposed configuration of feedback coil.

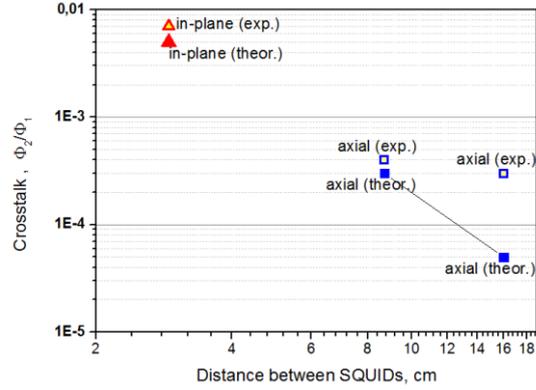


FIG. 3: Experimentally measured crosstalk for different positions of neighbouring sensors and corresponding estimations: (▲, ▲) for a coplanar orientation and (■, ■) for an axial orientation.

In order to take full advantage of high- T_c DC SQUIDs, they should be placed in a dense array as close as possible to the scalp and to neighbouring sensors. More than 100 encapsulated high- T_c DC SQUID magnetometers can be arranged around the head of an adult human. The problem is the variety of individual sizes of heads that should be accommodated in a mechanically adjustable MEG system to maintain close proximity of the sensors to the scalp.

The high- T_c sensors may be placed very close (< 3 mm) to the scalp by locating them in the vacuum space of the cryostat. In this case, the sensors are fixed inside thermal conducting sockets and cooled sideways, for example with the help of vacuum grease. The thermal radiation shields can be placed between the sensors and the warm wall. Alternatively, the sensors can be placed inside individual dimples on the other side of the cold wall, preferably immersed in liquid nitrogen.

When constructing the cryostat holder or gantry for a multichannel high- T_c MEG system, one should take into account the fact that the density of liquid nitrogen (~ 0.8 kg/liter) is much higher than that of liquid helium (~ 0.128 kg/liter). A typical 50 liter cryostat for MEG would be ~ 33 kg heavier if it would be filled with liquid nitrogen. This may require modifications of contemporary gantries for low- T_c MEG systems.

In conclusion, we have developed high- T_c DC SQUID magnetometers, which can be implemented in multichannel measurement systems for MEG, but construction of a cryostat of high- T_c MEG systems is still an issue.

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